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Phase behavior of graft copolymers in concentrated solution

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The phase behavior of graft copolymers dissolved in a graft-selective solvent was studied by using self-consistent field theory. The effects of polymer concentration and molecular architecture, *i.e.*, the number of junctions and the position of the first junction on the phase behavior were investigated. Phase diagrams were mapped out according to the calculation results. The detailed studies on the microstructures revealed that the graft copolymers can have either a local crosslinked structure or a global crosslinked structure, yielding a vital material for reversible physical gels. In addition, the density distributions and bridging fractions were calculated to understand the filling of solvents and packing of graft copolymers in the ordered structures of the gels. The understanding of the microstructures of graft copolymers in concentrated solution provides useful information for designing high-performance gels.

1 Introduction

Graft copolymers have attracted considerable attention because of their unique molecular architectures as well as their promising applications such as for coating and adhesive films.^{1–3} It is well established that the graft copolymers can self-assemble into classical microstructures, such as lamella, gyroid, hexagonally packed cylinders, and body-centered cubic spheres,^{4–10} as a consequence of microphase separation between backbones and graft arms. Within these microstructures, the continuous backbones provide the opportunities for the bridged chain conformations which combine different graft arm domains. The network resulted from bridged conformations can be applied to many structure designs. One application is that, when the network of graft copolymers is exposed to solvent, it is possible to generate a reversible physical gel in concentrated solution.¹¹ On the grounds of this consideration, the interest of the present work turns to the study of the graft copolymers in concentrated solutions, based on our previous works.^{6,12–14}

For two-component graft copolymers, the solvent is always selective due to different characteristics of the graft arms and the backbone. The solvent thus prefers to exist in the domain of one species rather than the other. This preference results in the formation of various microstructures, for example, micro-aggregates and physical gels. In addition, the particular architectures of graft copolymers also have an effect on the microstructures self-assembled from the copolymer/solvent system. Therefore, understanding the role of the solvent is

important for clarifying the phase behavior of graft copolymer solutions. However, there are only limited studies on this issue. For example, Nagahama *et al.* have investigated the phase behavior of poly(depsipeptide-*co*-lactide)-*g*-poly(ethylene glycol) (PDG-_{DL}-LA-*g*-PEG) copolymers in aqueous solution.¹⁵ Their concerns are focused on the sol–gel transitions. It was found that the sol–gel transition temperatures are greatly dependent on the concentration and the molecular architecture. In the theoretical study aspect, progress is less developed for explaining the phase behavior of graft copolymers in concentrated solution. Since graft copolymers have many influencing factors that determine their architectures, including the length of backbone, the length of graft arms, and the distribution of graft arms, a wide variation in hydrophobic–hydrophilic balance can be achieved and tuned to design the character of the systems. Due to their limited nature, the experiments can only give a narrow scope of the phase behavior of the graft copolymers in solution. Therefore, a comprehensive theoretical study is needed to provide a deep insight into the phase behavior of the graft copolymers in solution, and further guide the experimental studies.

SCFT (self consistent field theory) has emerged as a powerful tool to study the equilibrium thermodynamic features of polymer melts and concentrated polymer solutions.^{16–26} Drolet and Fredrickson have developed a numerical approach to solve the SCFT equations implemented in real space.^{4,27–30} Real-space SCFT is a highly expedient method for the study of copolymer phase behavior. The calculations can start from either random potential fields without a prior assumption about the mesophase symmetry²⁷ or a deterministic initial field possessing symmetry of order phases for accurate calculation of free energy.^{31,32} SCFT calculations for a blend can be performed in either the canonical ensemble or the grand-canonical ensemble.^{17,26,33} The combination of these two ensembles has a number of advantages on

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calculating the phase boundaries of the ordered phases and the two phase coexistence. The canonical algorithm is more stable because the volume fraction of each component is fixed, while the grand-canonical ensemble is more convenient to locate the two phase coexistence especially when the coexistence is narrow.²⁶ In our group, SCFT has been successfully used to study graft copolymers, including bridged chain conformation, phase behavior, and aggregate morphologies in dilute solution.^{6,12,13} In this work, we focus on the phase behavior of graft copolymers in concentrated solution which people have not investigated yet.

The purpose of present work is to study the phase behavior of graft copolymers in a graft-selective solvent, particularly in concentrated solutions. SCFT performed in both canonical and grand-canonical ensembles was applied in this study. Phase diagrams were mapped out to understand the influence of polymer concentration on phase behavior. In addition, the effect of first junction positions and junction numbers on the microstructures was also investigated. The results revealed that these microstructures are essentially crosslinked due to the continuous nature of the backbone, and thereby the systems can be used to design reversible physical gels. With this consideration in mind, bridging fractions were calculated to gain insight into the degree of crosslinking, which could be related to the mechanical properties of the physical gels.

2 Theory

We consider an incompressible blending system with volume V containing n_G graft copolymers **AB** and n_S solvent molecules **S**. Each copolymer is comprised of a flexible homopolymer **A** backbone along which m flexible homopolymer **B** graft arms are spaced. The position of i th graft arm located at τ_i is given by

$$\tau_i = \tau_1 + \frac{(i-1)(1-2\tau_1)}{m-1} \quad 1 \leq i \leq m \quad (1)$$

The copolymers are assumed to be monodisperse with a statistical length of a . The degrees of polymerization of the **A** and **B** chains are N_A and N_B , respectively. Thus, the total degree of polymerization of graft copolymer N_G is equal to $N_A + mN_B$. The volume fractions of **A**-type and **B**-type monomers of each copolymer chain are respectively denoted f_A and f_B . The volume fraction of graft copolymers in solution is c_P and that of the solvent is $1 - c_P$.

Within the mean-field theory, the configurations of a single copolymer chain and the solvent are determined by a set of effective chemical potential fields $w_K(\mathbf{r})$ ($K = \mathbf{A}, \mathbf{B}, \mathbf{S}$), replacing actual interactions within the solution. These potential fields are conjugated to the density field $\phi_K(\mathbf{r})$. We invoke an incompressibility ($\phi_A(\mathbf{r}) + \phi_B(\mathbf{r}) + \phi_S(\mathbf{r}) = 1$) by introducing a Lagrange multiplier $\xi(\mathbf{r})$. For a graft copolymer solution, in the canonical ensemble, the free energy (in units of $k_B T$), F_c , is given by

$$\begin{aligned} F_c = & -c_P \ln \left(\frac{Q_G}{c_P V} \right) - (1 - c_P) N_G \ln \left(\frac{Q_S}{(1 - c_P) V} \right) \\ & + \frac{1}{V} \int d\mathbf{r} [\chi_{AB} N_G \phi_A(\mathbf{r}) \phi_B(\mathbf{r}) + \chi_{AS} N_G \phi_A(\mathbf{r}) \phi_S(\mathbf{r}) \\ & + \chi_{BS} N_G \phi_B(\mathbf{r}) \phi_S(\mathbf{r}) - w_A(\mathbf{r}) \phi_A(\mathbf{r}) - w_B(\mathbf{r}) \phi_B(\mathbf{r}) \\ & - w_S(\mathbf{r}) \phi_S(\mathbf{r}) - \xi(\mathbf{r}) (1 - \phi_A(\mathbf{r}) - \phi_B(\mathbf{r}) - \phi_S(\mathbf{r}))] \end{aligned} \quad (2)$$

and in the grand-canonical ensemble, the free energy (in units of $k_B T$), F_{gc} , is

$$\begin{aligned} F_{gc} = & -\frac{Q_G}{V} - \frac{z Q_S}{V} + \frac{1}{V} \int d\mathbf{r} [\chi_{AB} N_G \phi_A(\mathbf{r}) \phi_B(\mathbf{r}) \\ & + \chi_{AS} N_G \phi_A(\mathbf{r}) \phi_S(\mathbf{r}) + \chi_{BS} N_G \phi_B(\mathbf{r}) \phi_S(\mathbf{r}) - w_A(\mathbf{r}) \phi_A(\mathbf{r}) - w_B(\mathbf{r}) \phi_B(\mathbf{r}) \\ & - w_S(\mathbf{r}) \phi_S(\mathbf{r}) - \xi(\mathbf{r}) (1 - \phi_A(\mathbf{r}) - \phi_B(\mathbf{r}) - \phi_S(\mathbf{r}))] \end{aligned} \quad (3)$$

where $z \equiv \exp(\mu/k_B T)$, and μ is the chemical potential.

Here, Q_S is the partition function for a solvent in the field $w_S(\mathbf{r})$, and is given by

$$Q_S = \int d\mathbf{r} \exp \left(-\frac{w_S(\mathbf{r})}{N_G} \right) \quad (4)$$

$Q_G = \int d\mathbf{r} q_A(\mathbf{r}, 1)$ is the partition function for a single non-interacting, grafted chain subject to the fields $w_A(\mathbf{r})$ and $w_B(\mathbf{r})$ in terms of backbone propagator $q_A(\mathbf{r}, s)$. The contour length s increases continuously from 0 to 1 as the block changes from one end of the chain to the other. The spatial coordinate \mathbf{r} is in units of R_A , where $R_A^2 = N_A a^2/6$.

The backbone propagator is divided into $m + 1$ segments

$$q_A(\mathbf{r}, s) = q_A^{(j)}(\mathbf{r}, s) \text{ for } \tau_j \leq s < \tau_{j+1} \quad j = 0, 1, \dots, m \quad (5)$$

$$\tau_0 \equiv 0 \quad \tau_{m+1} \equiv 1$$

where each segment satisfies the modified diffusion equation

$$\frac{\partial q_A^{(j)}(\mathbf{r}, s)}{\partial s} = \left[R_A^2 \nabla^2 - \frac{N_A}{N_G} w_A(\mathbf{r}) \right] q_A^{(j)}(\mathbf{r}, s) \quad (6)$$

and is subject to the following initial conditions:

$$q_A^{(j)}(\mathbf{r}, \tau_j) = q_A^{(j-1)}(\mathbf{r}, \tau_j) q_B(\mathbf{r}, 1) \quad j = 1, 2, \dots, m \quad (7)$$

$$q_A^{(0)}(\mathbf{r}, 0) = 1 \quad (8)$$

Here, $q_B(\mathbf{r}, s)$ is a propagator for **B** graft that satisfies the following modified diffusion equation:

$$\frac{N_A}{N_B} \frac{\partial q_B(\mathbf{r}, s)}{\partial s} = \left[R_A^2 \nabla^2 - \frac{N_A}{N_G} w_B(\mathbf{r}) \right] q_B(\mathbf{r}, s) \quad (9)$$

and is subject to the initial condition $q_B(\mathbf{r}, 0) = 1$ for the free end of the graft at $s = 0$. We also define a back-propagator of the j th **B** chain, $q_{B_j}^+(\mathbf{r}, s)$. It satisfies eqn (9) and starts on the end of the **B** chain tethered to the backbone. It is therefore subject to the initial condition

$$q_{B_j}^+(\mathbf{r}, 0) = \frac{q_A(\mathbf{r}, \tau_j) q_A(\mathbf{r}, 1 - \tau_j)}{q_B^2(\mathbf{r}, 1)} \quad (10)$$

In terms of these propagators, the densities are obtained by simple integration. They are obtained from

$$\phi_A(\mathbf{r}) = \frac{V c_P f_A}{Q_G} \sum_{j=1}^{m+1} \int_{\tau_{j-1}}^{\tau_j} ds q_A^{(j-1)}(\mathbf{r}, s) q_A^{(m+1-j)}(\mathbf{r}, 1 - s) \quad (11)$$

$$\phi_B(\mathbf{r}) = \frac{V c_P f_B}{m Q_G} \sum_{j=1}^m \int_0^1 ds q_B(\mathbf{r}, s) q_{B_j}^+(\mathbf{r}, 1 - s) \quad (12)$$

$$\phi_S(\mathbf{r}) = \frac{V(1 - c_P)}{Q_S} \exp\left[-\frac{w_S(\mathbf{r})}{N_G}\right] \quad (13)$$

in the canonical ensemble and from

$$\phi_A(\mathbf{r}) = f_A \sum_{j=1}^{m+1} \int_{\tau_{j-1}}^{\tau_j} ds q_A^{(j-1)}(\mathbf{r}, s) q_A^{(m+1-j)}(\mathbf{r}, 1 - s) \quad (14)$$

$$\phi_B(\mathbf{r}) = \frac{f_B}{m} \sum_{j=1}^m \int_0^1 ds q_B(\mathbf{r}, s) q_{Bj}^+(\mathbf{r}, 1 - s) \quad (15)$$

$$\phi_S(\mathbf{r}) = z \exp\left[-\frac{w_S(\mathbf{r})}{N_G}\right] \quad (16)$$

in the grand-canonical ensemble.

Finally, the minimization of the free energy F with respect to $\phi_A(\mathbf{r})$, $\phi_B(\mathbf{r})$, $\phi_S(\mathbf{r})$, and $\xi(\mathbf{r})$ leads to the set of mean-field equations

$$w_A(\mathbf{r}) = \chi_{AB} N_G \phi_B(\mathbf{r}) + \chi_{AS} N_G \phi_S(\mathbf{r}) + \xi(\mathbf{r}) \quad (17)$$

$$w_B(\mathbf{r}) = \chi_{AB} N_G \phi_A(\mathbf{r}) + \chi_{BS} N_G \phi_S(\mathbf{r}) + \xi(\mathbf{r}) \quad (18)$$

$$w_S(\mathbf{r}) = \chi_{AS} N_G \phi_A(\mathbf{r}) + \chi_{BS} N_G \phi_B(\mathbf{r}) + \xi(\mathbf{r}) \quad (19)$$

$$\phi_A(\mathbf{r}) + \phi_B(\mathbf{r}) + \phi_S(\mathbf{r}) = 1 \quad (20)$$

Next, we briefly describe the calculation method that determines the bridged and looped conformations of the backbones. Following the approach of Matsen³⁴ and our previous work,¹² we first evaluate the partition function,

$$\bar{q}_A(\mathbf{r}, s = \tau_i) = \begin{cases} q_A(\mathbf{r}, s = \tau_i) & \mathbf{r} \in D_1 \\ 0 & \text{elsewhere} \end{cases} \quad (21)$$

for the **A** backbone with its i th junction constrained to the first unit cell D_1 . For example, for cylinders with an **A**-forming matrix, the first unit cell D_1 can be obtained by performing a Voronoi tessellation with respect to the center of a cylindrical domain. The distribution can be now propagated by solving eqn (6) as the initial condition at $s = \tau_i$ up to $s = \tau_{i+1}$. The fraction of looped conformation, f_i , where the blocks between the i th junction and the $(i + 1)$ th junction have both ends in the cell D_1 , is given by³⁵

$$f_i = \frac{\int_{D_1} d\mathbf{r} \bar{q}_A(\mathbf{r}, \tau_{i+1}) q_A(\mathbf{r}, 1 - \tau_{i+1})}{\int_V d\mathbf{r} \bar{q}_A(\mathbf{r}, \tau_{i+1}) q_A(\mathbf{r}, 1 - \tau_{i+1})} \quad (22)$$

The average looped fraction, f_{loop} , for the cell D_1 is then obtained as

$$f_{\text{loop}} = \frac{1}{m-1} \sum_{i=1}^{m-1} f_i \quad (23)$$

The fraction of bridged conformation can be given by $f_{\text{bridge}} = 1 - f_{\text{loop}}$. An average value of f_{bridge} can be evaluated by repeating the calculation for all cells and calculating an arithmetic average.

To solve the SCFT equations, we used a variant of the algorithm developed by Fredrickson and co-workers.²⁷⁻³⁰ The

diffusion equations were solved with the Baker–Hausdorff operator splitting formula proposed by Rasmussen *et al.*^{36,37} To accurately determine the stable state and phase boundaries, we then start calculations from a deterministic initial field constructed from functions proportional to harmonics for the structures including the lamellar, hexagonally packed cylindrical, body-centered spherical, and bicontinuous gyroid phases.^{31,32,38,39} The stable structures are obtained by exhaustively comparing the free energy of the computed structures with the free energies of other structures. Because the regions of two phase coexistence are narrow in the phase diagram, it is difficult to map out these regions by calculating the free energies in canonical ensemble. Therefore, the free energies were equated in grand-canonical ensemble around the phase boundaries which were calculated in canonical ensemble, to obtain the two phase coexisting solutions.

All of the simulations were carried out in three dimensions. The spatial resolution Δx is set to be smaller than $0.10R_A$. It was found that the free energy of the system can be well converged to a stable value when Δx is smaller than $0.10R_A$. Contour step sizes for the **A** backbone and **B** graft arms were set at 0.01. The numerical simulations proceeded until the relative free energy difference was smaller than 10^{-6} and the incompressibility condition was achieved. Adjustment of the box size was used to minimize the free energy, as suggested by Bohbot-Raviv and Wang.⁴⁰ The box size corresponding to the lowest free energy upon convergence was chosen as the most appropriate one.

3 Results and discussion

As previous studied, the graft copolymer can self-assemble into aggregates such as vesicles and micelles in dilute solution.⁶ In the present work, we focused on another region where the solutions are in the concentrated state, by taking advantage of SCFT. SCFT was used to study the effect of polymer concentration on the phase behavior of graft copolymer solutions, and the corresponding phase diagrams were mapped out. Furthermore, detailed information such as density distribution and bridging fraction was analyzed to understand the role of polymer concentration in the ordered structures.

In the simulations, the polymerization degree of the graft copolymer N_G is assumed to be 40, and the volume fraction f_A of the backbone in each graft copolymer is taken to be 0.70. The backbone is hydrophobic to solvent **S** with $\chi_{AS} N_G = 56.0$, while the graft arm is hydrophilic to solvent **S** with $\chi_{BS} N_G = -4.0$. In addition, the interaction strength between the backbone and graft arms is set to be $\chi_{AB} N_G = 40.0$.

3.1 Phase diagram

Fig. 1 shows phase diagrams in relation to the first junction position and polymer concentration for the graft copolymer/solvent systems with $m = 2$ (Fig. 1a) and $m = 3$ (Fig. 1b). The phase diagrams contain four characteristic zones: a solvent-rich disordered phase (**Dis₁**), a microphase (lamella, gyroid, cylinder, and sphere), a polymer-rich disordered phase (**Dis₂**), and two phase coexistence (**2Φ**). When the volume fraction of polymer is very small, the graft copolymer is dissolved in solvent and a disordered solution rich in solvent is formed (**Dis₁**). As the volume fraction of polymer increases, the two phase coexistence

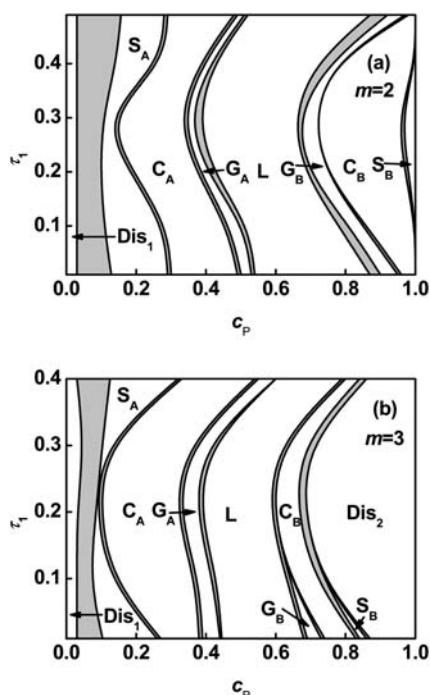


Fig. 1 Phase diagrams in τ_1 - c_P space for **AB** graft copolymers with $m = 2$ (a) and $m = 3$ (b) in solution. The ordered regions are denoted as **S** (body-centered cubic spheres), **G** (bicontinuous gyroid), **C** (hexagonally packed cylinders), and **L** (lamellae). The subscripts **A** and **B** in **S**, **G**, and **C** denote that the minority domains of ordered structure are formed by **A** and **B** blocks, respectively. The notes **Dis₁** and **Dis₂** refer to solvent-rich disordered phase and polymer-rich disordered phase, respectively. The light gray regions represent the region of two phase coexistence (2Φ).

region (2Φ) is formed. In this 2Φ region, aggregates with various microstructures such as micelles and vesicles appear. The detailed studies of the aggregates are reported in our previous work.⁶ As polymer concentration continues to increase, the diagram shows a microphase region. Ordered microstructures are formed in this region, on which we mainly focus. This microphase consists of lamellae, gyroids, cylinders, and spheres. The 2Φ phases appear between the adjacent ordered phases, and these two phase coexistence regions are smaller in contrast with the ordered phases. After passing a narrower 2Φ region, further increasing the concentration, a disordered solution rich in polymer emerges due to weak segregation of the graft copolymers (**Dis₂**). In the microphase region, when the polymer concentration c_P is small, the graft copolymer solution allows the possibility of forming reverse structures, such as gyroids, G_A , cylinders, C_A , and spheres, S_A . In these microstructures, the backbones are occupied in the minor domains, although the blocks of the backbone are the major component in the polymer. When the polymer concentration c_P becomes larger, the graft copolymers in solution form ordered microstructures such as spheres, S_B , cylinders, C_B , and gyroids, G_B , where the backbones form the continuous matrix and the grafts form the minor domains. Lamellar microstructures are found between G_A and G_B phases.

From the phase diagram, it is noted that the phase boundaries in the microphase show marked shifts: first to the left and then to the right as the τ_1 value increases. In the region of smaller τ_1 , with

increasing τ_1 , the boundaries tend to shift toward small values of c_P . On the contrary, increasing τ_1 gives rise to a shift toward larger values of c_P in the region of larger τ_1 . In the region of intermediate τ_1 , the effect of τ_1 on the boundaries is not significant. This behavior can be rationalized by considering the stretching energy of the chains.¹³ As can be seen from Fig. 1a and 1b, the regions of ordered structures and phase boundaries also have a marked change as the junction number increases 2 to 3.

Since junction number exerts a marked effect on the phase behavior, phase diagrams in junction number m versus polymer concentration c_P plane were also plotted at various τ_1 values. Fig. 2 illustrates phase diagrams for graft copolymers with $\tau_1 = 0.1$ and $\tau_1 = 0.3$. As shown in Fig. 2, the ordered region is shrunk with increasing m value due to dramatic enlargement of the polymer-rich disordered phase region. It can be attributed to the lower entropy of graft copolymer originated from the increasing of junction constraint.²⁶ The phase boundaries of **L-2Φ-G_B**, **G_B-2Φ-C_B**, **C_B-2Φ-S_B**, and **S_B-2Φ-Dis₂** shift towards smaller values of c_P as junction number m increases. The phase boundaries of **C_A-2Φ-G_A** and **G_A-2Φ-L** show a unique characteristic. The boundaries first shift toward smaller c_P values, then turn to larger c_P values, and finally shift to smaller c_P values as m increases when $\tau_1 = 0.1$ (Fig. 2a). However, when $\tau_1 = 0.3$ (Fig. 2b), the boundaries of **C_A-2Φ-G_A** and **G_A-2Φ-L** shift toward larger values of c_P as m increases from 2 to 4, and then toward smaller c_P values as m further increases to 5.

In our previous work,¹³ we investigated the phase behavior of graft copolymer melts. It was found that the ordered phase transition of **S_A → C_A → G_A → L → G_B → C_B → S_B** occurs as volume fraction of graft arms decreases and a unique shift of phase boundary takes place as the position of the first junction

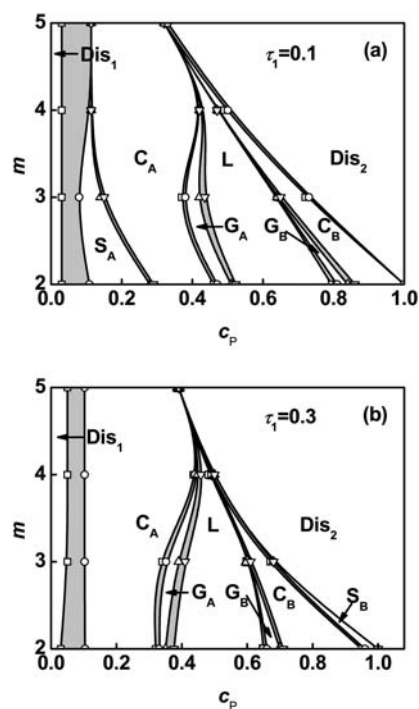


Fig. 2 Phase diagrams in m - c_P space for **AB** graft copolymers with $\tau_1 = 0.1$ (a) and $\tau_1 = 0.3$ (b) in solution. Labels appear as in Fig. 1.

changes (first to the left and then to the right as the value of τ_1 increases). Comparing with the present phase diagrams (Fig. 1 and Fig. 2) it is found that, in the concentrated solution, the decrease of the solvent volume fraction acts in a manner that corresponds qualitatively to the decrease of the volume fraction of grafts in bulk. This can be due to the fact that solvents behave as the fillers of grafts in concentrated solutions.

3.2 Density distribution

As stated above, solvents act as the fillers of graft arms in the ordered phase. However, how the solvents fill in the space of graft arms and further influence the distribution of graft copolymers under different molecular architectures is unknown. To address this question, we examined the density distributions of solvent, backbone, and graft arms for graft copolymer solutions. Fig. 3 shows the volume fraction profiles in a lamellar phase of graft copolymer with $m = 2$ and $\tau_1 = 0.1$ at various polymer concentrations c_p . The deviation of volume fraction profiles is $\Delta\phi_K = \phi_K - \bar{\phi}_K$, where $\bar{\phi}$ is the average volume

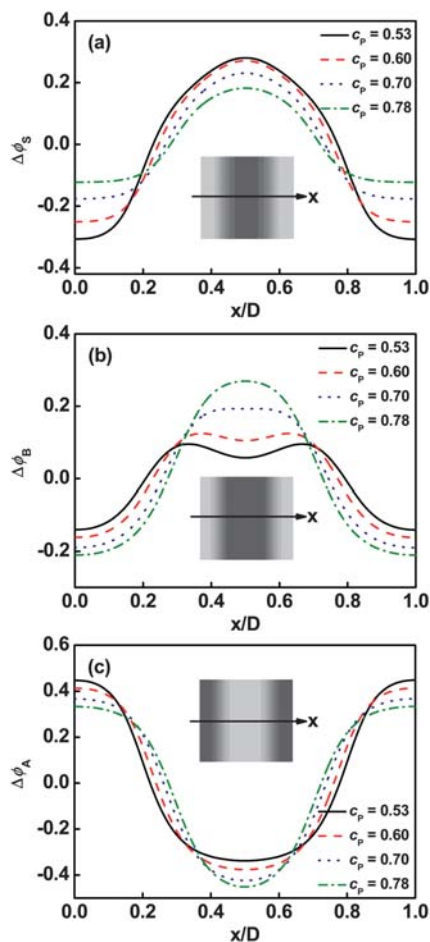


Fig. 3 Deviation of volume fraction profiles $\Delta\phi$ for S solvent (a), B blocks (b), and A blocks (c) on a cross section of the lamellar phase marked with an arrow in the inset at $m = 2$ and $\tau_1 = 0.1$. The inserts show the two-dimensional density distributions of S solvent (a), B graft arms (b), and A backbone (c). The colors ranging from black to gray in the inserts represent the densities from higher to lower.

fraction of component K ($K = A, B, S$). As shown in Fig. 3a, the solvents prefer to be distributed in the centers of B graft arm domains. It was found that the local deviation in solvent volume fraction in the center of B domains decreases with increasing polymer concentration. Fig. 3b shows the density distributions of B graft arms. When the polymer concentration is high, the density profile of B blocks has almost a plateau in the center regions. As the polymer concentration decreases, a cave in the center and two protrusions near the interface appear due to the increased amount of solvent in the center of the graft arm domains. In addition, the local deviation of A volume fraction in the center of its domains shows a decrease as the polymer concentration increases (Fig. 3c).

When the molecular architecture is varied, the graft copolymer distributions are also changed under the effect of the solvent. Fig. 4 shows the effect of the position of first junction τ_1 on the density distributions in the lamellar phase. As shown in Fig. 4a, the A block distributions are slightly broader at the intermediate value of τ_1 (0.30) relative to that at larger (0.45) or smaller (0.01) values, indicating the segregation between A domains and swollen B domains (B and S) are weaker at intermediate τ_1

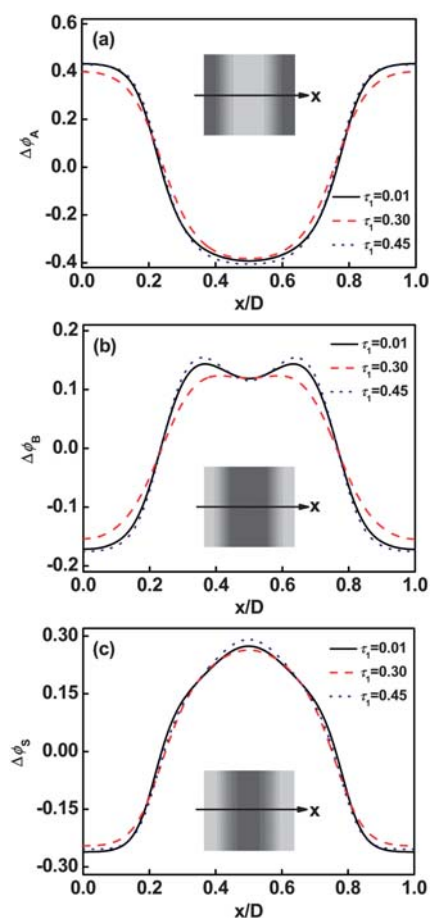


Fig. 4 Deviation of volume fraction profiles $\Delta\phi$ for A blocks (a), B blocks (b), and S solvents (c) on a cross section of the lamellar phase marked with an arrow in the inset at $m = 2$ and $c_p = 0.6$. The inserts show the two-dimensional distributions of A backbone (a), B graft arm (b), and S solvents (c). The colors ranging from black to gray in the inserts represent the densities from higher to lower.

values. A cave and two protrusions in **B** graft arm distribution curves were observed at smaller or larger τ_1 values due to the repulsion of solvent in the center of the **B** domains. However, plateau distribution is found at the intermediate τ_1 value (see Fig. 4b). This is due to the fact that the influence of solvent becomes less marked when the graft copolymer solutions are weakly segregated ($\tau_1 = 0.30$). The solvent distributions are also affected by τ_1 . The local deviation of solvent volume fraction in the center of **B** domains shows a slight decrease with increasing τ_1 from 0.01 to 0.3 and then turns to increase as τ_1 increases from 0.3 to 0.45 (see Fig. 4c).

The effect of the junction number on the density distribution is further examined. A representative result of the dependence of the deviation of volume fraction profiles $\Delta\phi$ in cylindrical phase **C_A** on m is shown in Fig. 5. As shown in Fig. 5a, with increasing m , the **A** distributions are broader and the local deviations of volume fraction in the center of its domains are decreased. For the deviations of **B** volume fraction, when m is small, a cave in the center and two protrusions near the interface are clearly viewed (Fig. 5b). However, when m is large, the protrusions in **B** distribution become flat and the nearly homogeneous **B**

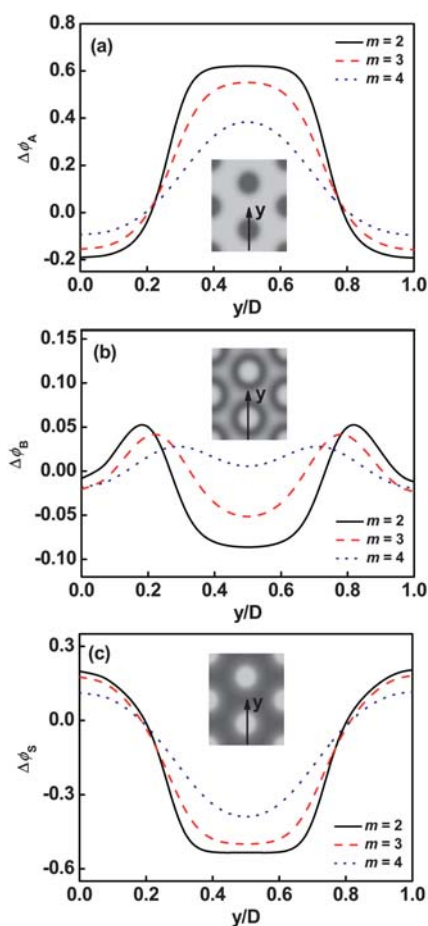


Fig. 5 Deviation of volume fraction profiles $\Delta\phi$ for **A** blocks (a), **B** blocks (b), and **S** solvent (c) on a cross section of the cylindrical phase marked with an arrow in the inset at $\tau_1 = 0.1$ and $c_p = 0.3$. The inserts show the two-dimensional density distributions of **A** backbone (a), **B** graft arm (b), and **S** solvents (c). The colors ranging from black to gray in the inserts represent the densities from higher to lower.

distribution was observed. It is attributed to weak segregation of the graft copolymer which results from the decreasing in the average interaction strength $\chi_{AB}N/m$,^{13,26} as the value of m increases. The weak segregation of graft copolymer leads to the broad distributions of **A** and **B** blocks in solution when m is larger. Moreover, the solvent distributions are also broader and the local deviation of volume fraction in the center of **B** domains decreases as m increases, which is shown in Fig. 5c.

3.3 Domain spacing

Domain spacing is also used to characterize the packing of graft copolymers and the filling of solvents. The results of the dependence of the domain spacing on the architecture parameter are presented in Fig. 6. Fig. 6a shows domain size $D/lan_A^{1/2}$ as a function of polymer concentration for graft copolymers with $m = 2$ at different values of τ_1 . The periods of the lamellar phase, gyroid phase, cylindrical phase, and spherical phase respectively are D , $6^{1/2}D$, $(4/3)^{1/2}D$, and $(3/2)^{1/2}D$ (D is the period of lamella, the size of the unit cell, the spacing between cylinders, and the spacing between the spheres, respectively). For each structure, the domain spacing tends to decrease with increasing polymer concentration, implying that the filling of solvents in graft arm domains increases the domain spacing. In addition, the domain sizes relatively decreases as τ_1 increases from 0.10 to 0.30. Fig. 6b illustrates the effect of junction number on the domain size $D/lan_A^{1/2}$. It is shown that a decrease in the domain size takes place as the junction number m increases. The variations of τ_1 and m values lead to the change of backbone asymmetry and thus the domain size. Furthermore, varying the polymer

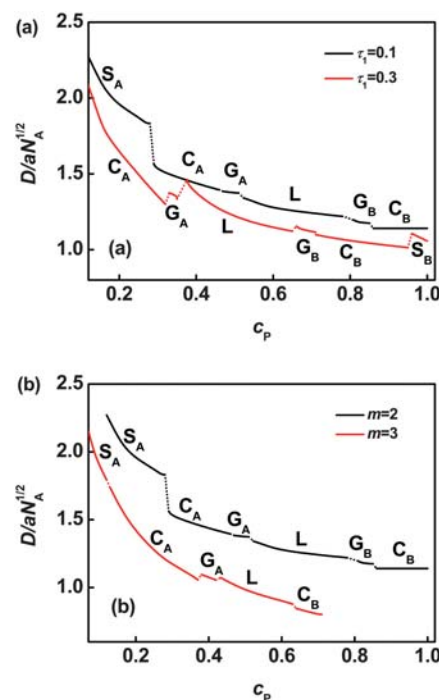


Fig. 6 Characteristic domain size $D/lan_A^{1/2}$ as a function of c_p for graft copolymers with $m = 2$ (a) and $\tau_1 = 0.10$ (b) in solution. Labels appear as in Fig. 1. The dash lines are drawn to link the solid lines when the graft copolymer solution is in the two phase coexistence state.

concentration is somewhat similar to changing volume fraction of graft arms.

3.4 Bridging fraction

Owing to the architectural characteristic of graft copolymers, the backbone can provide an association in the system. When the backbone occupies the minor domains, the graft copolymers form a local crosslinked structure with a connected core in swollen matrix, as shown in the scheme in Fig. 7a. The local crosslinked structures can be regarded as physical gels.¹⁵ Formation of such physical gels is supported by some experimental evidence. Nagahama *et al.* prepared a series of graft copolymers composed of hydrophilic poly(ethylene glycol) side-chains and a hydrophobic poly(depsipeptide-*co*-lactide) backbone (PDG-DL-LA-*g*-PEG).¹⁵ When the graft copolymers are dissolved in water, physical gels can be observed above a certain concentration. This is well in line with our prediction. As can be seen in Fig. 7a, the graft copolymers form physical gels when they are in concentrated solutions. The work of Nagahama *et al.* also suggests that the gels have hydrophobic PDG-DL-LA cores with hydrophilic PEG shells extended outside. The structural features of these physical gels are consistent with our theoretical predictions. As shown in the insets of Fig. 5, the hydrophobic backbone forms local crosslinked cores surrounded by swollen graft polymers, and simultaneously pack into an ordered structure that was observed in the experiments. In addition to these agreements with the experimental data, we predicted some behavior which have not yet been found. For example, the gel can separate into various microstructures, such as lamellae, cylinders, spheres, *etc.*, and the order-order transitions occur with increasing polymer concentration. These findings may provide a useful guidance for the further experimental observations.

With increasing graft copolymer concentration, a global crosslinked structure is formed, where the backbone exists in the matrix, as shown in Fig. 7b. The global crosslinking gives rise to a network, and thus a conventional polymer gel is formed. Crosslinking is the main feature of gels, and determines the properties such as mechanical properties and rheological behavior.¹¹ Therefore, it is important to understand the crosslinking in the global gels. As previous stated,¹² the backbone of graft copolymer can take chain conformations including tangles, loops whose junctions localize in the same domain, and bridges

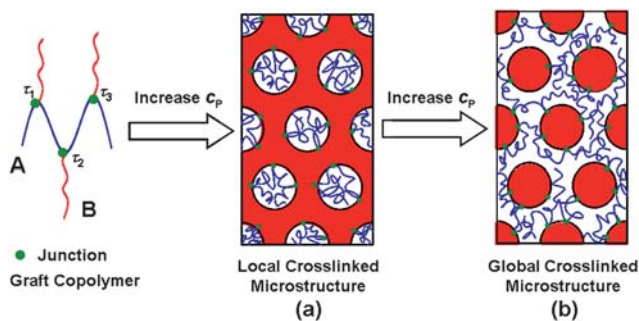


Fig. 7 Schematic illustration of chain conformations of graft copolymers as a function of polymer concentration. The solvents are not shown for clarity.

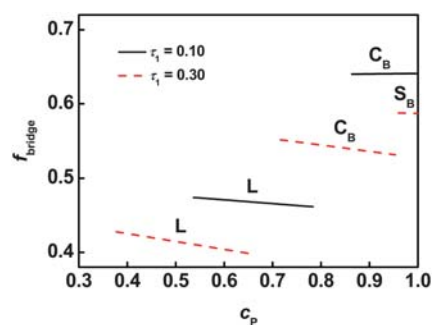


Fig. 8 Bridging fraction f_{bridge} as a function of the polymer concentration c_p for graft copolymer with $m = 2$ in solution.

whose junctions are anchored to different interface. In these conformations, only the bridged conformation makes contributions to global crosslinking. Therefore, the bridging fractions were calculated to clarify the structure of global crosslinked gels. Fig. 8 shows the equilibrium bridging fraction f_{bridge} plotted as function of the polymer concentration with $m = 2$. Typical results, for lamellar, cylindrical, and spherical structures, are presented. As the polymer concentration increases, the bridging fraction decreases slightly for each ordered structures. This implies that the effect of solvent on bridging fraction is less marked. In addition, the bridging fraction decreases with increasing τ_1 .

The bridging behavior can be further viewed in Fig. 9a where f_{bridge} is plotted against the first graft position τ_1 for graft

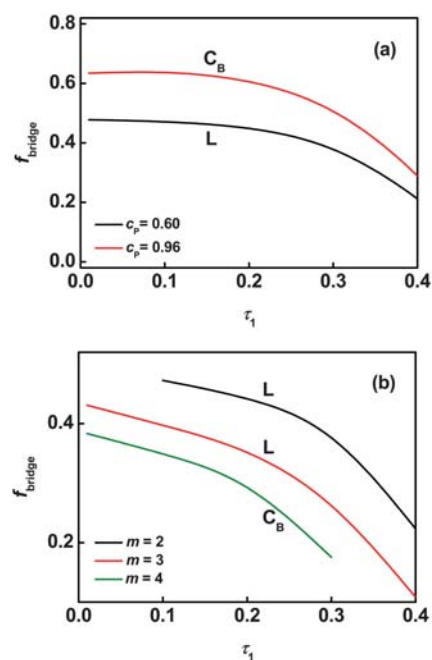


Fig. 9 Bridging fraction f_{bridge} as a function of the position of the first junction τ_1 in the lamellar phase ($c_p = 0.60$) and the cylindrical phase ($c_p = 0.96$) for graft copolymers with $m = 2$ (a). Bridging fraction f_{bridge} as a function of the position of the first junction τ_1 in the lamellar phase ($m = 2$ and 3) at $c_p = 0.60$ and the cylindrical phase ($m = 4$) at $c_p = 0.48$ for graft copolymer solutions (b).

copolymers with $m = 2$. It can be seen that f_{bridge} versus τ_1 has a slow drop over the range $0.01 \leq \tau_1 \leq 0.33$, and a rapid drop as τ_1 increases beyond 0.33 within a given ordered phase. The bridging fraction in the cylindrical phase ($c_P = 0.96$) is larger than that in the lamellar phase ($c_P = 0.60$). It is said that in phase C_B with smaller domain size, the backbone chains can take the bridging conformation more easily than when in phase L with larger domain size. As shown in Fig. 9b, the bridging fraction for gels decreases with increasing junction number at the same polymer concentration. This is because increasing the junction number shortens the block length between neighbor junctions on the backbone.

In general physical gels, such as the gels formed by triblock copolymers, each molecular chain can only provide a two-domain connection because the molecule only contains two crosslink points.^{41–43} The particular feature of graft copolymer gels is that the backbone of graft copolymer consists of multiple junctions, which can offer a multipoint connection more than two domains. Thus, a question arises about the maximum number of domains to which a single backbone is capable of connecting. To address this question, we calculated the possible junction point distributions in ordered phases. Fig. 10 shows a representative result obtained for the C_B phase with $m = 4$. We first determined the distribution of the first junction that is confined to a single minority B domain (0). This result is displayed in Fig. 10a. The associated second junction distribution

was then obtained by propagating that of the first junction (Fig. 10b). The bridges are formed, which starts from (0) domain and ends in other adjacent domains such as the (1), (2), and (3) domains. The third junction distribution was calculated with the second junctions confined to domain (1) (green frame in Fig. 10b), as shown in Fig. 10c. It was found that the third junctions appeared in the (2) and (6) domains as well as back to the (0) domain and the (1) domain itself. The fourth junction can also be propagated from the third junctions confined in domain (2) (blue frame in Fig. 10c). The fourth junction can exist in the new domain of (7) except for (0), (1), and (2) itself (Fig. 10d). These results indicate: the maximum number of the domains that a single backbone is able to connect is four and a possible conformation for the backbones to link four different domains is in the sequence of (0)–(1)–(2)–(7), as sketched in Fig. 10d. However, the volume fraction of fourth junction in the (7) domain is much lower, suggesting that the probability of simultaneously linking four distinct domains is small.

To further understand the crosslinking behaviors in the ordered structures, we calculated the probabilities of forming the bridged conformations that can respectively attach two, three, and more different swollen graft arm domains (n_{domains}), for each molecule. Fig. 11 shows a typical result for C_B phases. Obviously, the probabilities decrease as n_{domains} increases. For $m = 4$, it is almost impossible to link four different domains, suggesting that the backbone of graft copolymer is hard to take the complete bridged conformations. In addition, the increase in the value of τ_1 shows a marked effect on the decrease in the probability of bridges to link three domains. This means that the decrease in τ_1 is helpful for improving the total crosslinking. From the results of Fig. 10 and Fig. 11, we learned that for the C_B phase a single backbone is easy to connect three adjacent domains such as (0), (1) and (2) but difficult to connect an additional domain such as (7). The possibility of a graft copolymer chain simultaneously linking the three adjacent domains and other nearby domains is low.

The graft copolymers have attracted considerable attention because of their unique molecular architectures as well as their promising applications in various fields. The backbones of the graft copolymer in the gel provide the opportunities for the bridged chain conformation which combines different graft arm domains, resulting in various special usages such as enhanced mechanical properties. Our calculation results revealed that the

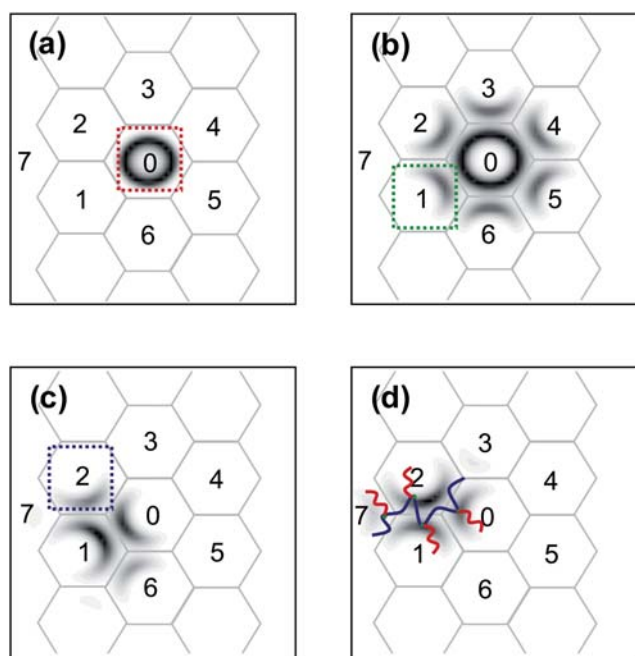


Fig. 10 Density plots of the first junction distributions that confined to a particular minority B domain (a), the second junction distributions (b) with the first junction confined in the domain (0) marked with the red frame shown in (a), the third junction distributions (c) with the second junction confined in the domain (1) marked with the green frame shown in (b), and the fourth junction distributions (d) with the third junction confined in the domain (2) marked with the blue frame shown in (c) for a cylindrical structure at $m = 4$, $c_P = 0.48$, and $\tau_1 = 0.1$. In (d), a possible conformation that the backbone links four different domains is sketched.

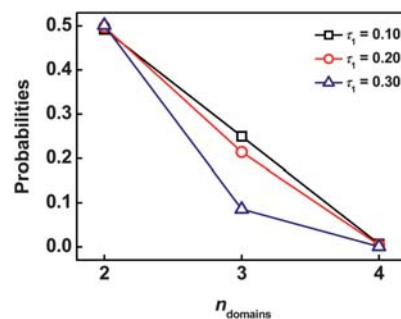


Fig. 11 Probabilities of simultaneously forming bridged connection for two, three, and four swollen B domains (n_{domains}) with $m = 4$ and $c_P = 0.48$ (for each backbone chain).

graft copolymers can have either a local crosslinked structure or a global crosslinked structure in concentrated solution. The molecular architecture and polymer concentration exert a profound effect on the microstructures. So far the theoretical understanding of the gel structure is limited, and most concern block copolymers such as linear multiblock copolymers which are capable of forming gels. Only very limited theoretical work is available for the phase behavior of the graft copolymers in concentrated solution. In comparison with the linear multiblock copolymers, the graft copolymers exhibit distinct advantages: 1) the microstructures of the linear multiblock copolymers always have global bridges, whichever component occupies the major domains. However, the graft copolymer chain can take either local bridged or global bridged conformation depending on the molecular architecture and polymer concentration. Therefore, the graft copolymer gel could have more controllable properties. 2) Comparing with the linear multiblock copolymers, the graft copolymers possess many more dangling graft arms, which are useful for further functionalization through connecting special chemical groups to the end of graft arms. This property is important in the applications in biomedical fields.

The unique characteristics of backbones can also be used to design more advanced materials, such as multicompartment physical gels, (the concept originated from the triblock copolymer gels⁴⁴) by attaching two or more dissimilar types of graft arms to the backbone. In such kind of gels, the backbones are forced to bridge two different types of micelles due to the mutually incompatible graft arms. Relative to present gel systems, the bridging fractions can be dramatically increased, resulting in an improvement of mechanical properties and rheological behavior. Additionally, introducing two mutual types of graft arms to the graft copolymers could enrich the microstructures of gels, thereby contributing to functional applications, for example, delivering simultaneously two drugs. The importance of the present work is that it not only helps us understand the nature of graft copolymer in concentrated solution but also offers useful information for designing high-performance gels.

4 Conclusions

We have studied the phase behavior of graft copolymers in a selective solvent using the self-consistent field theory. The influence of polymer concentration and molecular architectures was studied. Phase diagrams were mapped by comparing the free energy of different structures. It is found that the region of ordered phases is dependent on the architecture parameters (τ_1 and m), and regions of two phase coexistence appear between adjacent phases. When the polymer concentration increases, a sequence of $\text{Dis}_1 \rightarrow \text{S}_A \rightarrow \text{C}_A \rightarrow \text{G}_A \rightarrow \text{L} \rightarrow \text{G}_B \rightarrow \text{C}_B \rightarrow \text{S}_B \rightarrow \text{Dis}_2$ transitions, conjoined with two phase coexistence existed between two adjacent phases, was observed. In these phase transitions, the structures transform from local crosslinking to global crosslinking, exhibiting an interesting character related to physical gels. The detailed information regarding microscopic structures, including density distributions, domain size, and bridging fraction, was also reported for various molecular architectures. It was found that the graft copolymers can provide an opportunity for

multi-point crosslinking due to the fact that the backbone consists of multiple junctions, which may be helpful to enhance the mechanical properties of the physical gels, relative to widely-used physical gels such as triblock copolymer gels.

Acknowledgements

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